Plasmas Simulations Applied to the Study of Magneto-Aerodynamics Effects

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Abstract

A preliminary review of the literature about magnetoaerodynamics (MAD) is presented, focused on the study of super and hypersonic flow field of air plasmas generated by upstream focused laser energy deposition. The main phenomena which interplay in MAD are briefly discussed as well as some proposed models and difficulties in the related research areas. Alternative approaches and models are pointed-out.

Keywords: magneto-aerodynamics, finite element method, plasma simulation, particle-in-cell model, computational fluid dynamics.

1. Introduction

The study of aerodynamic drag reduction is of high interest in Aeronautic and Aerospace research. Many different approaches for magneto-aerodynamics (MAD) have been proposed and investigated both experimentally and computationally [18]. As a rule, the studies on this multidisciplinary research area require interplay of advanced the knowledge in electromagnetism, Aerodynamics, chemical and quantum Physics and Applied Mathematics. MAD typically requires high performance parallel computing.

Essentially, the physical modelling of a MAD problem consists in simulating an electrically conducting fluid flow in the presence of electric and magnetic fields. The electromagnetic field can properly modify the ionized gas flow. This means that the applied electromagnetic field interacts with the charged particles of the fluid and the gas flow can be, in certain way, controlled by that field. At hypersonic flight speeds, the air temperature is very high producing considerable ionization. Also laser energy deposition has been successfully used, as well as plasma injection, for both drag reduction and hypersonic flow control A. Passaro Laboratório de Engenharia Virtual M. A. S. Minucci Laboratório de Termodinâmica e Hypersônica Instituto de Estudos Avançados – IEAv/CTA, Brasil angelo@ieav.cta.b sala@ieav.cta.br

research. Additionally, one can consider externally applied electromagnetic fields interacting with the flow field of the plasma [18], which can be injected [17] or generated [16, 7]. Many difficulties arise when modeling all the physical phenomena involved in the process. "This interdisciplinary endeavor not only presents extremely complex sciences issues, but it demands a significant knowledge not completely available at present." This quote refers to MAD [18].

Experimental research has been developed at the Institute for Advanced Studies (IEAv/CTA). The present work proposes the use of computer simulations for the understanding of some of the physical phenomena involved in the aerodynamic drag reduction in a blunt body by means of air plasma generated by laser energy deposition.

2. Some Challenges and Methodologies

The induced air spike, caused by the laser energy deposition, produces shock waves that can favorably interact with the flow field, while the plasma expands and is dragged over the body. Successive laser pulses are needed in order to continuously generate the plasma. These processes can be didactically associated to some research areas, such as plasma generation, MAD, and laser-plasma interactions. Many potential new contributions can arise in the analysis, modeling and simulation of some of the involved phenomena, as shown in next subsections.

2.1 Plasma generation

One of the main issues on using plasma upstream in a blunt body is that the shock wave envelope in the plasma field exhibits an outward displacement compared to a simple gas dynamic shock [18]. However, the study of the possible effects on the flow field of an ionized fluid (plasma) under the action of external electromagnetic fields requires an accurate assessment of the intrinsic properties of the plasma, which are difficult to determine either theoretically or experimentally [18]. Some models have been proposed for simulating the air breakdown caused by a laser beam [8, 9, 23]. These simulations can provide the input required for simulating the plasma expansion, leading to a more accurate initial configuration of the particle system.

2.2 Plasma expansion

After the air breakdown, the plasma is dragged by the flow field, which might be modeled by MHD equations. However, the required inputs for solving these equations include the physical properties of the fluid (the plasma). For this purpose, a collisional Particle-In-Cell (PIC) model [6, 13, 20] can be adopted to simulate the evolution of the charged particles and to determine the required physical properties of the medium. The PIC methodology indirectly solves the Vlasov equation by separately solving the Maxwell Equations for the fields and the Newton's motion equations [4]. The Maxwell equation is solved for an initial configuration of the particle system, using as inputs the charge and current densities at the nodal points. The computed fields are then interpolated at the particle positions and, by means of the Lorentz force equation, the motion equations are integrated. The Maxwell equations are usually solved by a Finite Difference Method (FDM) and a Spectral Method. However, recent works show the successful coupling of the Finite Element Method (FEM) with the PIC model [14, 15]. In this case, the Newton's equations can be integrated using an Euler method [5] or a leapfrog scheme [14, 15].

2.3 Magneto-Hydrodynamics (MHD)

The modeling of the plasma flow in the presence of electric and magnetic fields combines both the Maxwell and Navier-Stokes equations, which leads to a very complex set of equations. Although characteristic-based methods like approximate-Rieman [18] are often used for solving this set of equations, we intend to adopt a recently reported stabilized FEM approach [21]. Other methods may be considered for solving the full Navier-Stokes equation, such as discontinuous Galerkin methods [1, 2, 3,] or element-free Galerkin methods [10, 21].

2.3.1 Governing Equations

The governing equations can be written in the following flux vector form:

$$\frac{\partial \mathbf{V}}{\partial t} + \frac{\partial \mathbf{F}_x}{\partial x} + \frac{\partial \mathbf{F}_y}{\partial y} + \frac{\partial \mathbf{F}_z}{\partial z} = \frac{\partial \mathbf{F}_{x,r}}{\partial x} + \frac{\partial \mathbf{F}_{y,r}}{\partial y} + \frac{\partial \mathbf{F}_{r,z}}{\partial z}$$
(1)

where $\mathbf{V} = (\rho, \rho u, \rho v, \rho w, \rho E, B_x, B_y, B_z)^T$ is the vector of conservative dependent variables. The flux vectors $\mathbf{F}_{x,r}$, \mathbf{F}_y , and $\mathbf{F}_{z,r}$ are associated with the resistivity, heat transfer and viscous dissipation, thereby, in the case of ideal MHD¹ the right hand side of Eq. (1) is identically null. The ideal MHD equations can be written as:

$$\frac{\partial \mathbf{V}}{\partial t} + \frac{\partial \mathbf{F}_x}{\partial x} + \frac{\partial \mathbf{F}_y}{\partial y} + \frac{\partial \mathbf{F}_z}{\partial z} = 0.$$
 (2)

The FEM discretization can be written as:

$$\left(\int_{\Omega} \mathbf{N}^{T} \mathbf{N} d\Omega\right) \Delta \overline{\mathbf{V}} = -\Delta t \left\{ \int_{\Omega} \frac{\partial \mathbf{N}^{T}}{\partial x_{i}} \left(\mathbf{F}_{i}^{n+\frac{1}{2}} + \mathbf{G}_{i}^{n} \right) d\Omega + \int_{\Gamma} \mathbf{N}^{T} \left(\mathbf{F}_{i}^{n+\frac{1}{2}} + \mathbf{G}_{i}^{n} \right) \mathbf{n}_{i} d\Gamma \right\}$$
(3)

where, **N** represent the FEM base functions, **F** corresponds to the ideal MHD flux and **G** to the non ideal model ($\mathbf{G}_i = \mathbf{F}_{ir}$) [21]. However, the standard Galerkin procedure leads to spurious numerical oscillations in the velocity and pressure solutions, for advection dominated flows. These instabilities can be reduced or even eliminated by applying some stabilization method, like the Stream-line upwind Petrov-Galerkin (SUPG) and Galerkin Least Squares. For instance, the SUPG stabilization term is introduced by considering a Petrov-Galerkin weight function of the form:

$$\mathbf{W} + \tau \mathbf{A}_k^T \frac{\partial \mathbf{W}}{\partial x_k}, \qquad (4)$$

where, $\mathbf{A}_{k} = \frac{\partial \mathbf{F}_{k}}{\partial \mathbf{V}}$, (5)

and τ is a matrix calculated at the element level and is dependent on a suitable defined element length and the local velocity, in each direction [12]. A well detailed derivation of the flux vector form for the MAD equations, as well as the details of the FEM discretization and the resulting stabilized SUPG weak form can be found in [21].

2.4 Laser – Plasma interaction

Since we are interested in maintaining the drag reduction, which is due to shock waves and electromagnetic interactions, the plasma must be generated continuously. Different models can be employed for this phenomena and the choice of the model depends on the effects that must investigated. In some situations, a gas dynamic based model can be used, while in others, effects such as absorption and scattering effects must be considered in order to find an optimized rate for the laser pulse. Depending on the plasma density, the laser energy can be scattered or

¹ The ideal MHD equations consider a physical model where the conductivity is assumed infinite, and viscosity and heat transfer is neglected.

absorbed. The modeling of air plasma generation by electron beams is an open area of research [7, 9, 19, 23].

3. Computational methodologies

The computational cost involved in the described simulations is high, since both the number of particles and of nodal variables required for adequately representing the system are enormous. Parallel computing becomes mandatory.

We obtained an excellent speed-up and efficiency with an object-oriented parallel PIC-FEM code developed for a distributed memory parallel machine [15]. Although in this implementation collisional effects were not modeled, the code can be easily modified in order to model these effects by means of a Monte-Carlo (MC) approach, called PIC-MC or PIC-MCC (PIC-MC Collision) [6, 13, 20].

The FEM formulations for the full MAD equations and for the Maxwell field equations result in large sparse linear systems depending on the size of the mesh. High performance parallel codes are also required for resolving these large systems. Moreover, it is necessary to employ costly adaptive strategies for adequately solving the shock waves interactions for the MHD flow field. Furthermore, discontinuous and *p*adaptive formulations [2] may be required, as well as alternative methods, such as the meshfree methods [10, 22].

Finally, the generality of the mathematical formulations and models allows to simulate many interesting phenomena in MAD, such as power extraction, flow control and design optimization.

4. References

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